## References

<sup>1</sup> Heppenheimer, T. A., "Optimal Controls for Out-of-Plane Motion about the Translunar Libration Point," *Journal of Space-craft and Rockets*, Vol. 7, No. 9, Sept. 1970, pp. 1087-1092.

<sup>2</sup> Farquhar, R. W., "Lunar Communications with Libration-Point Satellites," Journal of Spacecraft and Rockets, Vol. 4, No.

10. Oct. 1967, pp. 1383-1384.

<sup>3</sup> Farquhar, R. W., "Station-keeping in the Vicinity of Collinear Libration Points with an Application to a Lunar Communications Problem," Space Flight Mechanics, Science and Technology Series, American Astronautical Society, New York, 1967, Vol. 11, pp. 519-535.

<sup>4</sup> Porter, J. D., "Final Report for Lunar Libration Point Flight Dynamics Study," NASA GSFC Contract NAS-5-11551, April

1969, General Electric Co., Philadelphia, Pa.

## Reply by Author to R. W. Farquhar

T. A. Heppenheimer\*
University of Michigan, Ann Arbor, Mich.

 $\mathbf{F}^{\mathrm{ARQUHAR's}}$  comment on the fuel consumption estimates deserves a reply. In his Comment, Eq. (5) properly states the geometrical effects which define  $A_z$ ; let the value thus computed be denoted  $A_z'$ . Equation (7),

which is due to the present author, defines a value which is denoted  $A_{\varepsilon}^{h}$ . Then,

$$A_z^f/A_z^h = 1 + \frac{1}{2}(\sin\psi_c/k)^2 + 0(1/k^4)$$

Thus,  $A_z^h$  may be regarded as a lower bound, which is approximated for moderate values of k. Indeed, k = 3.0 gives  $(A_z^t/A_z^h) = 1.03$  for  $\Delta t = 93$  days. Nevertheless,  $A_z^t$  should indeed be used, and I thank Dr. Farquhar for his comment.

## Errata: "Effects of Products of Inertia on Re-Entry Vehicle Roll Behavior"

Albert E. Hodapp Jr. and Edward L. Clark Jr. Sandia Laboratories, Albuquerque, N. Mex.

[J. Spacecraft Rockets 8, 155-161 (1971)]

N the above paper, 1) Eq. (6) should read

$$\dot{p} = (1/I_X)\{M_X + (1/I)[J_{XY}(M_Y - I_Xpr) + J_{XZ}(M_Z + I_Xpq)]\}$$

2) in the section labeled "Conclusion," 2d should read "are zero at zero roll rate"; and 3) in the nomenclature, the fifth symbol defined should be  $C_{ma}$  not  $C_{m}$ .

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<sup>\*</sup> National Science Foundation Fellow, Department of Aerospace Engineering. Associate Member AIAA.

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